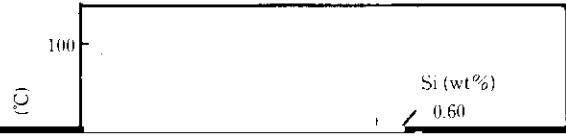
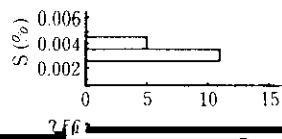
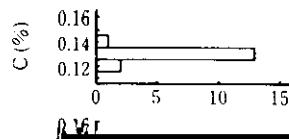


Hydrogen Attack in Cr-Mo Steels and Pitting of Austenitic Stainless Steel



Synopsis:

The characteristics of a hydrogen attack on $2\frac{1}{4}$ Cr-1 Mo steels were studied. Resistance to the hydrogen attack



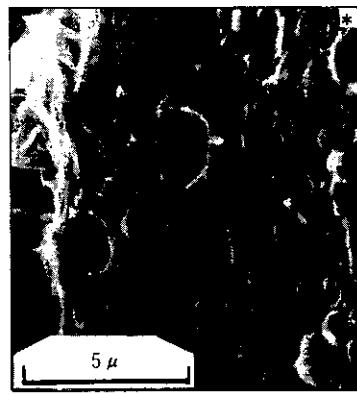
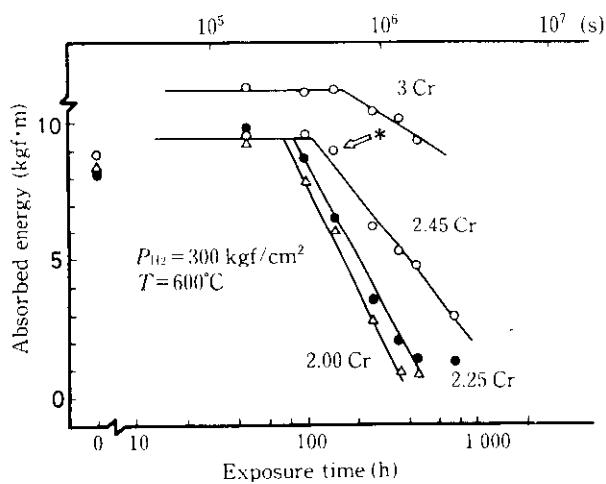


Fig. 3 Changes in absorbed energy during high temperature and high pressure hydrogen atmosphere, showing the effect of chromium content on the deterioration of toughness

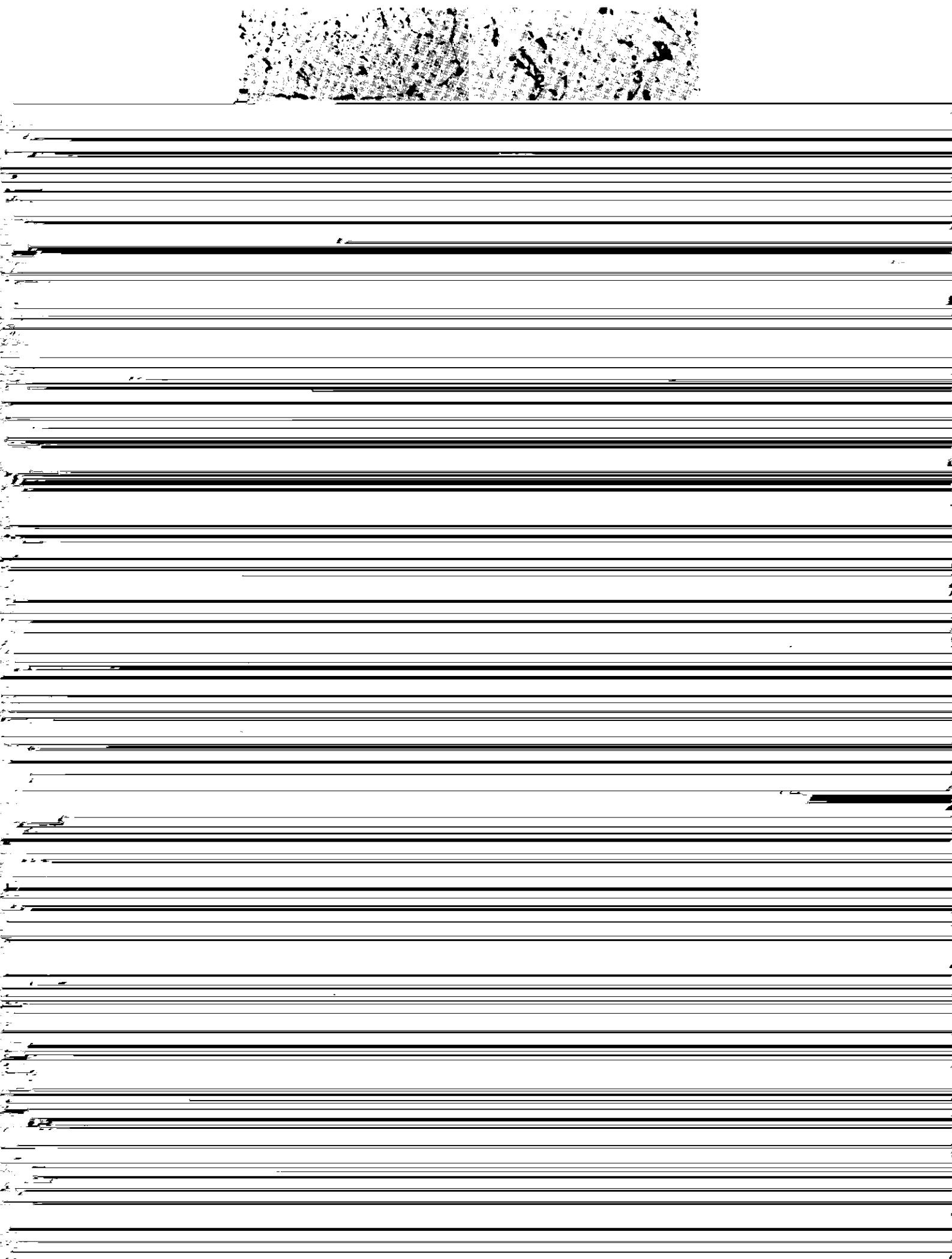
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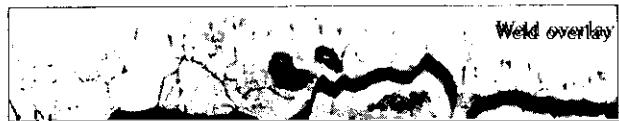
$P_{H_2} = 300 \text{ kg/cm}^2$
 $T = 600^\circ\text{C}$

ductile mode.

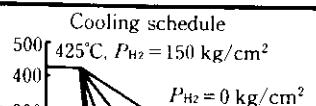
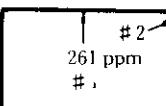
2.2 Shape of Carbides^{1, 2, 5)}

Diamond-like carbides in the $\alpha + \beta$ and γ regions of $\text{Fe}-\text{Cr}-\text{Al}-\text{C}$ steels



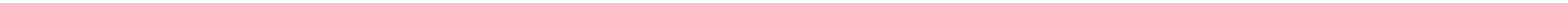


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ANSWER The answer is 1000.

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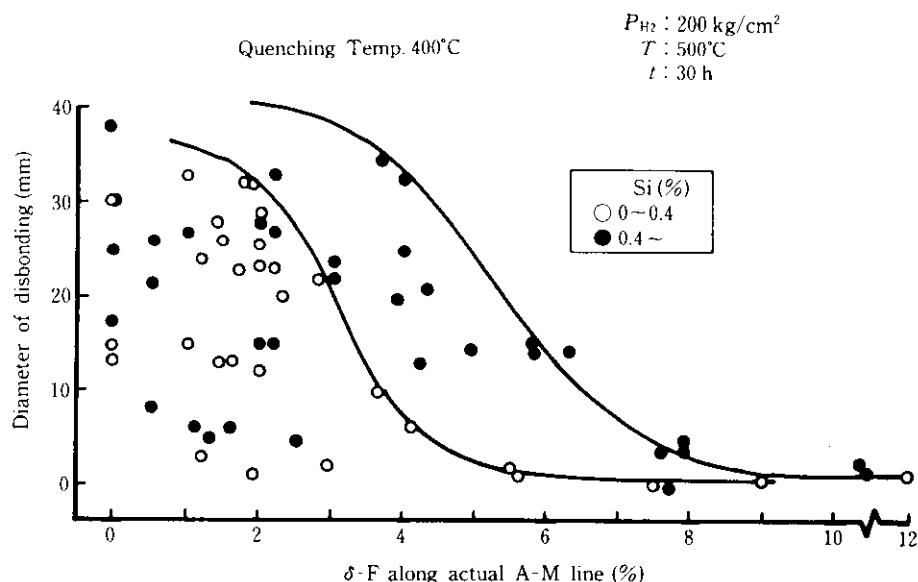
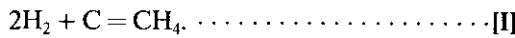


Fig. 9. Influence of silicon contents and δ -ferrite contents in mild steel on disbonding.

is essentially caused by the reaction:



When this reactin occurs inside steel, methane is trapped at the phase boundaries, forming voids which eventually grow and link, developing into large cracks.

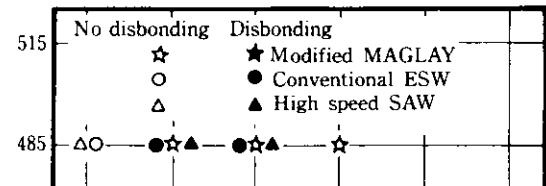
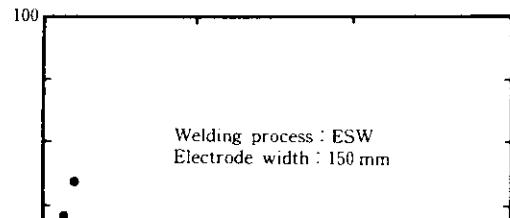
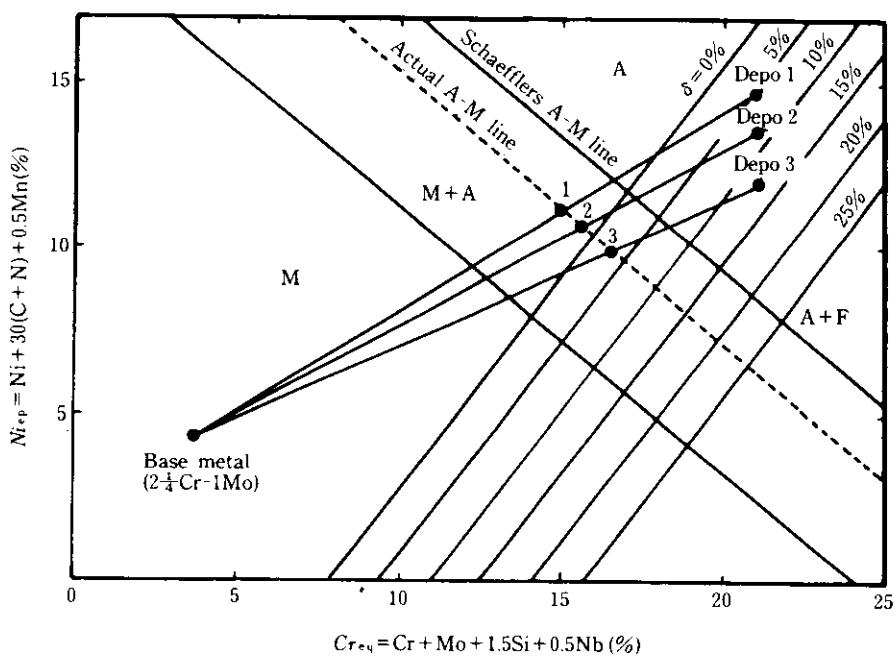
hydrogen, respectively. The above-mentioned effect of

Si on the kinetics of hydrogen attack and the significant effect of a slight Cr content difference on susceptibility to hydrogen attack must be explained by a difference in K^{II} in Eq. (7).

The partial pressure of methane is decisively

$$\Delta G^{\circ} = -16520 + 12.25T \log T$$

Hence, f_{CH_4} is 211 kgf/cm^2 for 2Cr-1Mo steel and



which properly controls the Si and δ -ferrite contents ensures the production of weld metal excellent in disbonding resistance.

No. 941, 2nd ed., API, June (1977)

- 5) T. Imanaka: "Effect of Cr Content on Hydrogen Attack of Cr-Mo Steels", *Preprint of Fall Meeting of the Japan Institute of Metals*, (1984), p. 469
- 6) F. K. Naumann: "Der Einfluß von Legierungszusätzen auf