



# Ferroalloy Production by Smelting Reduction Process with Coke-Packed Bed\*



*Synopsis:*

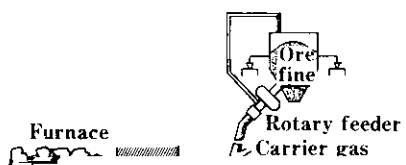
*A new smelting reduction process with coke-packed bed*

72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88
Fluidized bed reduction (iron ore)																



(a) Without acceleration

the fine ore without acceleration and shorter reduc



tion time.

#### 4 Fundamental Studies and Bench Scale Test

##### 4.1 Smelting Reduction Behavior in a

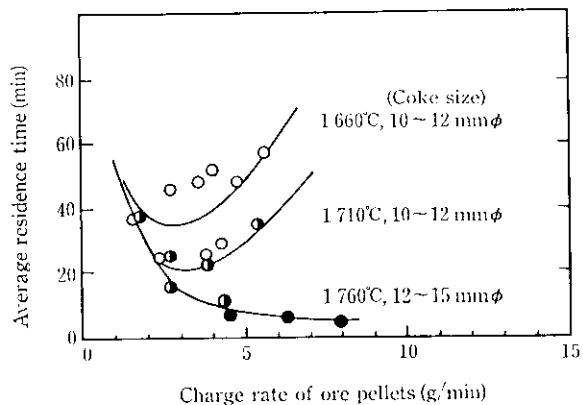


Fig. 5 Effect of the charging rate of ore on the average residence time in the coke-packed bed

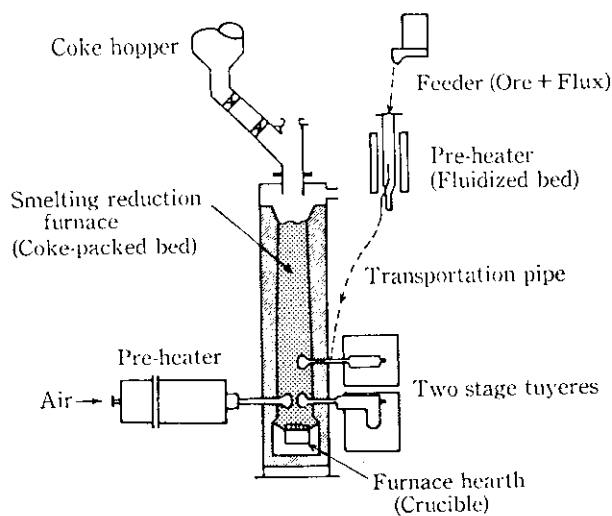


Fig. 6 Schematic diagram of the bench scale smelting reduction furnace

dependent on coke size. When the coke size is larger

to be almost the same as with a cold model test. This observation suggested that the coke size should be larger than 14 mm.

Figure 5 shows the effect of the ore charging rate on the average residence time. Average residence time is a function of ore charging rate, coke size, heat supply, and bed height. Initially, average residence time

O <sub>2</sub> in Pre-blast red.ratio	21%	26%	30%
0%		●	
10-30%	△	○	□
50%		⊗	

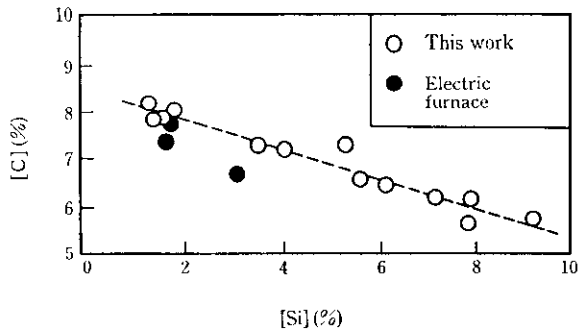
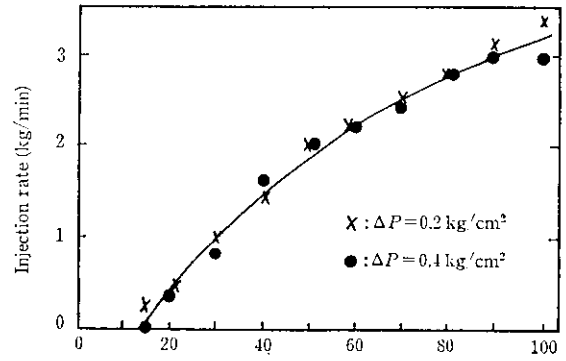


Fig. 9 Relation between C and Si content in metal



Fluidizing gas (NI/min)  
 Fig. 10 Influence of the fluidizing gas amount on the ore injection rate

### 4.3 Gravitational Ore Transportation System

One of the fundamental features of the STAR process is the direct injection of fine ore into the smelting reduction furnace through the upper tubes. The abra-

containers were regarded as a pre-reduction furnace and

sion of the transportation tubes and injection tubes is a serious problem with the conventional pneumatic powder transportation system, and may become even more serious when hot pre-reduced ore is used. Thus, the realization of a practical STAR process required develop-

smelting reduction furnace respectively. As the ore flow rate control device, a small fluidized bed was used, in which the flow rate of the ore was controlled by the amount of fluidizing gas. The effects of fluidizing gas volume, transport pipe scale, etc., on the realized pow-

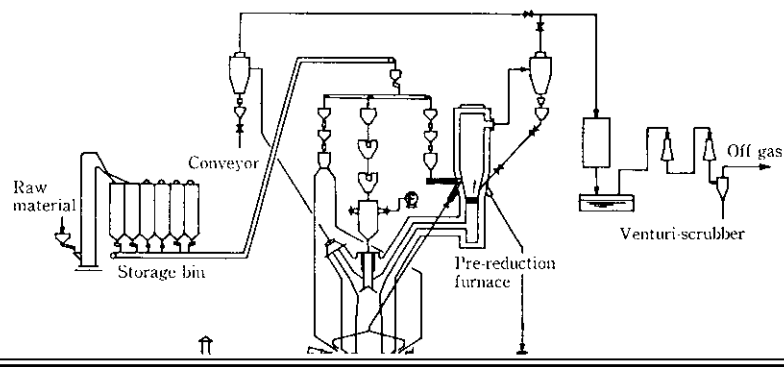


Table 1 Operation tests of pilot plant

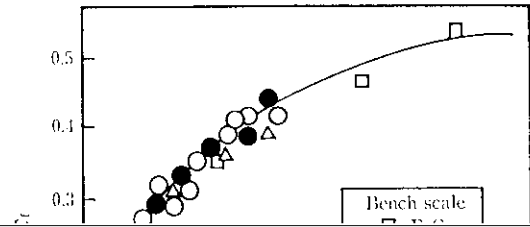
Top gas temperature varied in the range from 700°C to 1000°C, and was mainly dependent on the coke ratio

No.	Time	Temperature (°C)	Gas composition (%)	Yield (%)	Remarks
1	10:00	750	CO 12, H <sub>2</sub> 10, CH <sub>4</sub> 5, C <sub>2</sub> H <sub>6</sub> 2, C <sub>3</sub> H <sub>8</sub> 1, N <sub>2</sub> 69	10	Normal operation
2	11:00	800	CO 15, H <sub>2</sub> 12, CH <sub>4</sub> 6, C <sub>2</sub> H <sub>6</sub> 3, C <sub>3</sub> H <sub>8</sub> 2, N <sub>2</sub> 62	12	Normal operation
3	12:00	850	CO 18, H <sub>2</sub> 14, CH <sub>4</sub> 7, C <sub>2</sub> H <sub>6</sub> 4, C <sub>3</sub> H <sub>8</sub> 3, N <sub>2</sub> 59	14	Normal operation
4	13:00	900	CO 20, H <sub>2</sub> 16, CH <sub>4</sub> 8, C <sub>2</sub> H <sub>6</sub> 5, C <sub>3</sub> H <sub>8</sub> 4, N <sub>2</sub> 57	16	Normal operation
5	14:00	950	CO 22, H <sub>2</sub> 18, CH <sub>4</sub> 9, C <sub>2</sub> H <sub>6</sub> 6, C <sub>3</sub> H <sub>8</sub> 5, N <sub>2</sub> 55	18	Normal operation
6	15:00	1000	CO 24, H <sub>2</sub> 20, CH <sub>4</sub> 10, C <sub>2</sub> H <sub>6</sub> 7, C <sub>3</sub> H <sub>8</sub> 6, N <sub>2</sub> 53	20	Normal operation
7	16:00	950	CO 22, H <sub>2</sub> 18, CH <sub>4</sub> 9, C <sub>2</sub> H <sub>6</sub> 6, C <sub>3</sub> H <sub>8</sub> 5, N <sub>2</sub> 55	18	Normal operation
8	17:00	900	CO 20, H <sub>2</sub> 16, CH <sub>4</sub> 8, C <sub>2</sub> H <sub>6</sub> 5, C <sub>3</sub> H <sub>8</sub> 4, N <sub>2</sub> 57	16	Normal operation
9	18:00	850	CO 18, H <sub>2</sub> 14, CH <sub>4</sub> 7, C <sub>2</sub> H <sub>6</sub> 4, C <sub>3</sub> H <sub>8</sub> 3, N <sub>2</sub> 59	14	Normal operation
10	19:00	800	CO 15, H <sub>2</sub> 12, CH <sub>4</sub> 6, C <sub>2</sub> H <sub>6</sub> 3, C <sub>3</sub> H <sub>8</sub> 2, N <sub>2</sub> 62	12	Normal operation
11	20:00	750	CO 12, H <sub>2</sub> 10, CH <sub>4</sub> 5, C <sub>2</sub> H <sub>6</sub> 2, C <sub>3</sub> H <sub>8</sub> 1, N <sub>2</sub> 69	10	Normal operation
12	21:00	700	CO 10, H <sub>2</sub> 8, CH <sub>4</sub> 4, C <sub>2</sub> H <sub>6</sub> 1, C <sub>3</sub> H <sub>8</sub> 0.5, N <sub>2</sub> 76.5	8	Normal operation



Table 2 An example of heat balance and parameter  $E_f$  of the pilot plant test

	Zone I	Zone II	Zone III
Input	4 890 kcal/h	8 930 kcal/h	980 kcal/h



fluidity and melting point of slag by the adjustment of slag composition.

- (2) A gravitational powder transportation system was developed to feed fine ore to the smelting reduction furnace.
- (3) Operating and equipment conditions for upscaling the process can be estimated from the heat utilization parameter.
- (4) The production cost of ferrochromium on a com-

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